

### A Statistical Model for Estimating the Effect of Process Variations on Crosstalk Noise <u>M. Martina</u>, G. Masera CERCOM-Dip. Elettronica Politecnico di Torino



# Agenda

Introduction
Proposed Method
Experimental Results
Conclusions



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## Introduction

- The interconnects analysis in modern deep sub-micron technologies can not be faced with traditional analysis methodologies.
- Statistical analysis seems to be a good solution to obtain early prediction about interconnects non-ideal phenomena (e.g. cross-talk, delay, ...).



# Introduction

- To obtain a good prediction:
  - a good electrical model is required, combining accuracy and computational efficiency.
  - parasitic parameters must be available from 2D/3D extraction.
  - switching activities and time windows are required for all aggressor lines.



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# Case of study

• We concentrate on the case of coupled lines laying at the same metal level



 Current work is dealing with process variations and their impact on cross-talk noise.



### Problem formulation - I

- Considering the cross-talk noise voltage as a function  $V_x(t)=g(t,p_1, p_2, ..., p_n)$  of n statistically independent parameters  $(p_i)$ .
- Supposing each parameter exhibits a normal distribution  $p_i \sim N(\mu_{pi}, \sigma_{pi})$  (e.g. Cc ~  $N(\mu_{Cc}, \sigma_{Cc})$ ).
- We can consider any time value t for this analysis, since we concentrate on synchronous systems we pose t = t<sub>s</sub>.



## Problem formulation - II

- Starting from the statistical distribution of interconnects electrical parameters (R, C, Cc), we would like to obtain a closed form approximation of the statistical distribution of the cross-talk voltage.
- Two approaches can been pursued:
  - Approximating the voltage curve with an exponential function.
  - Representing the voltage expression as a partial second order Taylor expansion.



# Requirements

- This method needs:
  - To know the statistical distribution of interconnects electrical parameters.
  - The electrical parameters to be statistically independent.
  - A closed form expression of the cross-talk voltage on the victim line.



## CAVEAT

- A first order Taylor expansion would lead to the sum of Gaussian variables.
- Mixed second order Taylor expansion term are not considered  $(\partial^2 V / \partial p_i \partial p_j) \rightarrow$  it is not treatable as a closed form.
- Electrical parameters independence: actually it not true, however it is a simple case and a starting point to validate the methodology.



## **Proposed Method**

- Let's introduce a new set of random variables x<sub>i</sub>=p<sub>i</sub>-E[p<sub>i</sub>]
- Associating a random variable  $h = V_x(t_s)$ to the cross-talk voltage and taking a partial second order Taylor exapansion we obtain:





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#### Experimental results - I

Tech: 0.18  $\mu$ m R<sub>driver</sub> = 470  $\Omega$ Line = 3 mm Rising time = 10 ps Sampling period = 1 ns C<sub>c</sub> variation = 30% C<sub>a</sub>, C<sub>v</sub> variation = 20%





### Experimental results - II

Tech: 0.18  $\mu$ m R<sub>driver</sub> = 470  $\Omega$ Line = 5 mm Rising time = 10 ps Sampling period = 1 ns C<sub>c</sub> variation = 30% C<sub>a</sub>, C<sub>v</sub> variation = 20%





### Experimental results - III

Tech: 0.18  $\mu$ m R<sub>driver</sub>= 470  $\Omega$ Line = 5 mm Rising time = 10 ps Sampling period = 5 ns C<sub>c</sub> variation = 30% C<sub>a</sub>, C<sub>v</sub> variation = 20%





### **Experimental results - III**

Tech: 0.13  $\mu$ m R<sub>driver</sub>= 470  $\Omega$ Line = 3 mm Rising time = 10 ps Sampling period = 1 ns C<sub>c</sub> variation = 30% C<sub>a</sub>, C<sub>v</sub> variation = 20%





### **Experimental results - IV**

Tech: 0.13  $\mu$ m R<sub>driver</sub> = 470  $\Omega$ Line = 5 mm Rising time = 10 ps Sampling period = 1 ns C<sub>c</sub> variation = 30% C<sub>a</sub>, C<sub>v</sub> variation = 20%





### Experimental results - V

Tech: 0.13  $\mu$ m R<sub>driver</sub> = 470  $\Omega$ Line = 5 mm Rising time = 10 ps Sampling period = 5 ns C<sub>c</sub> variation = 30% C<sub>a</sub>, C<sub>v</sub> variation = 20%





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## Conclusions - I

- A statistical model for the evaluation of the cross-talk depending on process variations has been proposed
- Even if some assumptions are rather rough, preliminary results are interesting



# Conclusions - II

- The following actions are planned
  - Taking into account parameters correlation
  - Trying the proposed model on more complex structures
  - Developing models based on pure numerical-simulative approach
  - Concentrate on the cross-talk delay phenomenon



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Proposed Method - II

• For 2 lines we obtain:

 $h \gg h_0 + a_1 x_1 + a_2 x_2 + b_1 x_1^2 + b_2 x_2^2$ 

• Since  $h = V_x(t_s)$ , the cross-talk voltage statistical distribution can be evaluated from:  $F_h(z) = P(h \ f \ z)$ 

 $= P(\mathbf{h}_{0} + a_{1}\mathbf{x}_{1} + a_{2}\mathbf{x}_{2} + b_{1}\mathbf{x}_{1}^{2} + b_{2}\mathbf{x}_{2}^{2} \mathbf{f} \mathbf{z})$ 



### Proposed Method - III

• We can introduce

 $\mathbf{z}_i = a_i \mathbf{x}_i + b_i \mathbf{x}_i^2$ 

•  $\eta$  statistical distribution can be obtained from  $\zeta_i$  distribution:

 $P(\mathbf{h} \mathbf{f} z) = P(\mathbf{h}_0 + \mathbf{z}_1 + \mathbf{z}_2 \mathbf{f} z)$ 



Proposed Method - IV

• So

- If b > 0  $P(z \pounds z) = P(a\mathbf{x}+b\mathbf{x}^{2} \pounds z) = P(z_{1} \pounds \mathbf{x} \pounds z_{2})$ - If b < 0  $P(z \pounds z) = P(a\mathbf{x}+b\mathbf{x}^{2} \pounds z) = P(\mathbf{x} \pounds z_{2})+P(\mathbf{x} \overset{3}{z} z_{1})$ • Where  $z_{1}$  and  $z_{2}$  are the roots of  $b\mathbf{x}^{2}+a\mathbf{x}-z = 0$ 



## Proposed Method - V

Since p<sub>i</sub> where assumed to be gaussian and independent x<sub>i</sub>=p<sub>i</sub>-E[p<sub>i</sub>] are gaussian and independent with μ<sub>i</sub> = 0

- If b > 0

$$F_{z}(z) = P(z \mathbf{f} z) = F_{x}(z_{2}) - F_{x}(z_{1})$$

- If b < 0

$$F_{z}(z) = P(z \ \pounds \ z) = F_{x}(z_{2}) + 1 - F_{x}(z_{1})$$



Proposed Method - VI

 To obtain the probability density function (pdf) of η we can calculate ζ pdf.

 $f_z(z) = dF_z(z)/dz$  $f_z(z) = 1/\mathbf{D}[f_x(z_2) - f_x(z_1)]$ • Where  $\Delta = \sqrt{(a^2 + 4bz)}$ 



## Proposed Method - VII

• Thus if  $\theta = \zeta_1 + \zeta_2$  $f_q(z) = f_{z_1}(z) * f_{z_2}(z)$ • So since  $\eta = \eta_0 + \theta$ 

 $f_{\mathbf{h}}(\mathbf{y}) = f_{\mathbf{q}}(\mathbf{z} - \mathbf{h}_{0})$